Development of Corrosion Inhibitors Used in Acidization of Petroleum Oil Well

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ABSTRACT

An important method of protecting metallic materials against deterioration due to corrosion is by the use of corrosion inhibitors. In the present investigation, corrosion inhibition study of two amino acid compounds, 2-amino-N-decyl-3-phenylpropionamide (Inh I) and 2-amino-N-decylpropionamide (Inh II) have been performed for oil-well tubular steel (N-80) in 15% HCl using weight loss, electrochemical polarization and SEM techniques. The inhibition efficiencies of the inhibitors follow the sequence, Inh I > Inh II. The results showed that inhibition efficiency of all inhibitors increased with increase in inhibitors concentration. Both inhibitors act as mixed inhibitors and obey the Langmuir adsorption isotherm. Corrosion inhibition mechanism followed the adsorption phenomenon.

Keywords: Amino acid compounds; N80 steel; 15% HCl; Corrosion inhibition.

INTRODUCTION

Acidization of a petroleum oil well is one of the important stimulation techniques for enhancing oil production. It is commonly brought about by forcing a solution of 15% to 28% hydrochloric acid into the well to open up near bore channels in the formation and hence to increase the flow of oil. To reduce the aggressive attack of the acid on tubing and casing materials (N-80 steel), inhibitors are added to the acid solution during the acidifying process. Organic compounds containing polar groups including nitrogen, sulphur, oxygen and heterocyclic compounds with polar functional groups and/or conjugated double bonds have been reported as good corrosion inhibitors [1-11]. The effective acidizing inhibitors that are usually found in commercial formulations are acetylenic alcohols, alkenyl phenones, aromatic aldehydes, nitrogen-containing heterocyclics, quaternary salts and condensation products of carbonyls and amines[12-17]. However, these inhibitors suffer from drawbacks, they are effective only at high concentrations and they are harmful to the environment due to their toxicity, so it is important to search for new nontoxic and effective organic corrosion inhibitors for N-80 steel – 15% hydrochloric acid system. In this regard, amino acid compounds have a promising alternative for the design of eco-friendly corrosion inhibitors which will satisfy the environmental requirements.

Thus, it was considered interesting to prepare amino acid compounds like 2-amino-N-decyl-3-phenylpropionamide (Inh I) and 2-amino-N-decylpropionamide (Inh II) and to assess their inhibitive properties for oil-well tubular steel (N-80) in 15% hydrochloric acid.

MATERIALS AND METHODS

Materials
The working electrode and specimens for weight loss experiments were prepared from oil-well N-80 steel sheets having the following percentage composition:
Weight measurements

The specimens for the weight loss experiments were of the size 3 cm x 3 cm and those for electrochemical studies the size of the electrodes was 1 cm x 1 cm with a 4 cm long tag for electrochemical contact. Both sides of the specimens were exposed for both the techniques. The specimens were mechanically polished successively with 1/0, 2/0, 3/0 and 4/0 grade emery papers. After polishing with the paper of each grade, the surface was thoroughly washed with soap, running tap water, distilled water and finally was degreased with acetone. The samples were dried and stored in a vacuum dessicator before immersing in the test solution. For weight loss experiments 300 mL of 15% hydrochloric acid was taken in 500 mL glass beakers with lids. The inhibition efficiencies were evaluated after a pre-optimized time interval of 6 h using 10, 20, 50, 100 and 150 ppm of inhibitors. The specimens were removed from the electrolyte, washed thoroughly with distilled water, dried and weighed. The inhibition efficiencies were evaluated using the formula

\[
\% \text{IE} = \frac{w - w_i}{w} \times 100
\]

where, \(w\) is weight loss in absence of inhibitor and \(w_i\) is weight loss in presence of inhibitor.

Electrochemical measurements

The electrochemical experiments were carried out in a three necked glass assembly containing 150 mL of the electrolyte with different concentrations of inhibitors (from 10 ppm to 150 ppm by weight) dissolved in it. The potentiodynamic polarization studies were carried out with N80 steel strips having an exposed area of 1 cm\(^2\). A conventional three electrode cell consisting of N80 steel as working electrode, Platinum as counter electrode and a saturated calomel electrode as reference electrode was used. Polarisation studies were carried out using VoltaLab 10 electrochemical analyser and data was analysed using Voltamaster 4.0 software. The potential sweep rate was 10 mVs\(^{-1}\). All experiments were performed at 25 ± 0.2°C in an electronically controlled air thermostat. For calculating %IE by electrochemical polarization method we use the formula-

\[
\% \text{IE} = \frac{I_0 - I_{inh}}{I_0} \times 100
\]

Where, \(I_0\) = Corrosion current in absence of inhibitor
\(I_{inh}\) = Corrosion current in presence of inhibitor

Synthesis of inhibitors

The inhibitors were synthesized in the laboratory by amidation of methyl esters of amino acids with alkyl amine without solvents [18].

RESULTS AND DISCUSSION

Weight loss study

The percentage inhibition efficiencies (% IEs) of 10, 20, 50, 100 and 150 ppm Inh I and Inh II have been evaluated by weight loss technique at 25°C and the results are summarized in Table 1. It is evident from these values that both the inhibitors are significantly effective even at low concentrations like 10 ppm and there is a linear increase in %IE in the whole range of concentrations studied. The structure of the inhibitors are given below-
Table 1: Percentage inhibition efficiency (% IE) values calculated by weight loss technique for Inh I and Inh II at 25°C

<table>
<thead>
<tr>
<th>Concentration</th>
<th>Inh I (%IE)</th>
<th>Inh II (%IE)</th>
</tr>
</thead>
<tbody>
<tr>
<td>0</td>
<td>-</td>
<td>-</td>
</tr>
<tr>
<td>10</td>
<td>62.94</td>
<td>55.12</td>
</tr>
<tr>
<td>20</td>
<td>70.52</td>
<td>64.12</td>
</tr>
<tr>
<td>50</td>
<td>80.95</td>
<td>72.56</td>
</tr>
<tr>
<td>100</td>
<td>85.16</td>
<td>80.61</td>
</tr>
<tr>
<td>150</td>
<td>89.38</td>
<td>83.16</td>
</tr>
</tbody>
</table>

Electrochemical studies

Electrochemical polarization behaviour of Inh I and Inh II for N80 steel in 15% hydrochloric acid at 25°C is shown in figures 1 to 2 and various parameters obtained are given in tables 2 to 3.

![Electrochemical polarization curves](image)

**Figure 1:** Electrochemical polarization curves for N80 steel in 15% hydrochloric acid without (1), with 10 ppm (2), 20 ppm (3), 50 ppm (4) 100 ppm (5) and 150 ppm (6) of Inh I at 25°C

On the basis of observed IE values the inhibitors follow the order

Inh I > Inh II

The above order may be explained well considering adsorption of the inhibitor molecules on the metal surface through the probable sites of adsorption, N, S, O and phenyl ring. The participation of phenyl ring during the adsorption of the inhibitor may be shown by higher IE values in case of Inh I.

The curves in figures 1 and 2, illustrate that the nature of the curve remains almost same even after the addition of the inhibitors and also on increasing the concentration of the inhibitor. However, on increasing the concentration of the inhibitor the curves are gradually shifted towards lower current density. The corrosion potential also slightly shifted towards negative direction on increasing the concentration of the inhibitors. It is realized from these observations that the inhibitors molecules retard the corrosion process without changing the mechanism of corrosion.
process in the medium of investigation[19]. The magnitude of the shift in current density is directly proportional to the concentration of the inhibitors, indicating that the inhibitive property of the inhibitor is concentration dependent. It is clear from the polarization curves of the inhibitors that the shift in current density towards lower current density for anodic as well as cathodic curve increases on increasing the concentration of the inhibitor.

![Figure 2: Electrochemical polarization curves for N80 steel in 15% hydrochloric acid without (1), with 10 ppm (2), 20 ppm (3), 50 ppm (4) 100 ppm (5) and 150 ppm (6) of Inh II at 25°C](image)

The positive shift in the $E_{\text{corr}}$ in presence of inhibitors on increasing the concentration of the inhibitors is due to the decrease in the rate of anodic reaction. Moreover, the increase in the cathodic and anodic Tafel slopes ($\beta_c$ and $\beta_a$) are related to the decrease in both the cathodic and anodic currents. Both the inhibitors affect both, the anodic as well as cathodic sites, so these are mixed inhibitors.

**Table 2: Corrosion parameters obtained from polarization curves shown in Fig. 1 for N80 steel in 15% hydrochloric acid in the absence and presence of inhibitor Inh I.**

<table>
<thead>
<tr>
<th>Concentration (ppm)</th>
<th>$E_{\text{corr}}$ (mV)</th>
<th>$I_{\text{corr}}$ ($\mu$A cm$^{-2}$)</th>
<th>$\beta_c$ (mV dec$^{-1}$)</th>
<th>$\beta_a$ (mV dec$^{-1}$)</th>
<th>% IE</th>
</tr>
</thead>
<tbody>
<tr>
<td>0</td>
<td>-470</td>
<td>575</td>
<td>150</td>
<td>130</td>
<td>-</td>
</tr>
<tr>
<td>20</td>
<td>-468</td>
<td>219</td>
<td>167</td>
<td>153</td>
<td>62.32</td>
</tr>
<tr>
<td>50</td>
<td>-466</td>
<td>161</td>
<td>171</td>
<td>157</td>
<td>71.88</td>
</tr>
<tr>
<td>100</td>
<td>-464</td>
<td>109</td>
<td>173</td>
<td>159</td>
<td>80.32</td>
</tr>
<tr>
<td>150</td>
<td>-463</td>
<td>81</td>
<td>174</td>
<td>162</td>
<td>86.18</td>
</tr>
<tr>
<td>200</td>
<td>-460</td>
<td>69</td>
<td>175</td>
<td>161</td>
<td>88.48</td>
</tr>
</tbody>
</table>

**Table 3: Corrosion parameters obtained from polarization curves shown in Fig. 2 for N80 steel in 15% hydrochloric acid in the absence and presence of inhibitor Inh II.**

<table>
<thead>
<tr>
<th>Concentration (ppm)</th>
<th>$E_{\text{corr}}$ (mV)</th>
<th>$I_{\text{corr}}$ ($\mu$A cm$^{-2}$)</th>
<th>$\beta_c$ (mV dec$^{-1}$)</th>
<th>$\beta_a$ (mV dec$^{-1}$)</th>
<th>% IE</th>
</tr>
</thead>
<tbody>
<tr>
<td>0</td>
<td>-470</td>
<td>575</td>
<td>150</td>
<td>130</td>
<td>-</td>
</tr>
<tr>
<td>20</td>
<td>-467</td>
<td>253</td>
<td>165</td>
<td>156</td>
<td>56.12</td>
</tr>
<tr>
<td>50</td>
<td>-466</td>
<td>195</td>
<td>167</td>
<td>158</td>
<td>66.08</td>
</tr>
<tr>
<td>100</td>
<td>-464</td>
<td>144</td>
<td>170</td>
<td>160</td>
<td>74.96</td>
</tr>
<tr>
<td>150</td>
<td>-462</td>
<td>104</td>
<td>171</td>
<td>162</td>
<td>81.92</td>
</tr>
<tr>
<td>200</td>
<td>-460</td>
<td>92</td>
<td>172</td>
<td>164</td>
<td>84.02</td>
</tr>
</tbody>
</table>

The inhibition efficiencies calculated from the polarization data are in good agreement with those obtained from and weight loss measurement.

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Adsorption Isotherms

The adsorption of inhibitor molecules on the surface of the corroding metal has been considered as the root cause of corrosion inhibition. Assuming that the percentage area covered by the inhibitors is directly proportional to retardation in the corrosion rate, the compounds should obey Langmuir adsorption isotherm [20]. Langmuir isotherm may be written as

\[
\log \frac{\theta}{1 - \theta} = \log A + \log C - \frac{Q}{2.3RT}
\]

where \(A\) and \(Q\) are temperature independent constant and heat of adsorption respectively. The validity of Langmuir isotherm is confirmed from the linearity of the \(\log \frac{\theta}{1 - \theta}\) vs \(\log C\) plot having the slope value to be unity. The plots of \(\log \frac{\theta}{1 - \theta}\) vs \(\log C\) for the investigated inhibitors at 25°C are shown in Fig. 3. It is observed that although these plots are linear, the gradient are never unity, contrary to what is expected for the ideal Langmuir adsorption isotherm equation. The departure in the values of the slopes of Langmuir plots from unity may be advocated to be due to the mutual interaction between adsorbed molecules in a close vicinity [21]. Organic molecules and metal complexes having polar atoms or groups which are adsorbed on the metal surface may interact by mutual repulsion or attraction and hence may affect the heat of adsorption. All the inhibitors follow the Langmuir adsorption isotherm, indicating that the adsorption of inhibitors at the surface of N-80 is the root cause of corrosion inhibition.

Fig.3 : Langmuir plots
Microscopic Study
Figure 4 (a, b, c, ) show the microphotographs for N80 steel in 15% hydrochloric acid in the absence and presence of 150 ppm of Inh I at 200 X magnification. On comparing these micrographs, it appears that in the presence of inhibitor, the surface of the test material has improved remarkably with respect to its smoothness. The smoothening of the surface would have been caused by the adsorption of inhibitor molecules [22] on it and thus, the surface is fully covered.

![Microphotographs](image)

Fig. 4: SEM of (a) Polished sample (b) Sample in presence of 15% hydrochloric acid (c) Sample in presence of 150ppm of Inh I.

CONCLUSION

(i) Both the inhibitors Inh I and Inh II act as efficient corrosion inhibitor for N-80 steel in 15% HCl solution.
(ii) Inh I shows appreciably higher efficiency than the Inh II due to presence of more number of active centres and larger size as compared to the inhibitor Inh II.
(iii) Electrochemical polarization shows that both the the inhibitors act as mixed inhibitors.

It is suggested from the results obtained from SEM and Langmuir adsorption isotherm that the mechanism of corrosion inhibition is occurring through adsorption process.

REFERENCES